

# **KISSsoft 03/2016 – Instruction 102**

**Consideration of the deformation of a planet carrier**

**Step by step instructions**

**KISSsoft AG**

Rosengartenstrasse 4  
8608 Bubikon  
Switzerland

Tel: +41 55 254 20 50  
Fax: +41 55 254 20 51  
info@KISSsoft.AG  
www.KISSsoft.AG

# Contents

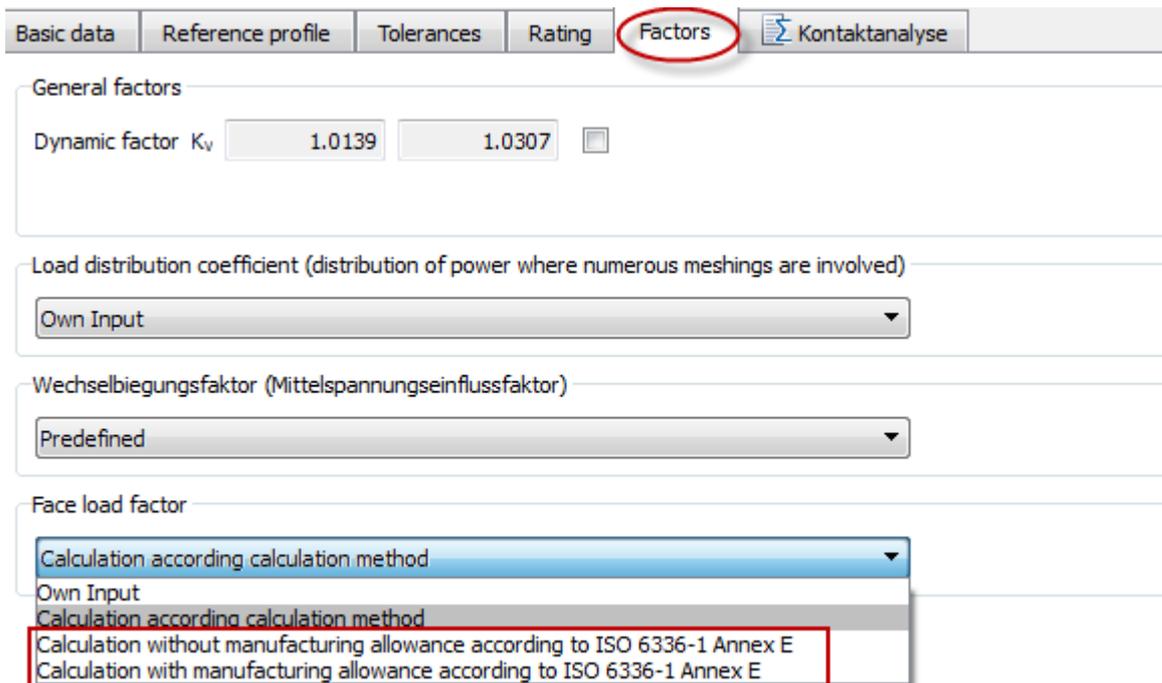
1	Introduction .....	3
2	Step by step instructions.....	3
3	General comments.....	12
	Annex 1. Comparison between the deformations of a single-sided and double-sided planet carrier .....	13

# 1 Introduction

Since KISSsoft 2015 version, the misalignment of a planet pin in the planet carrier due to the deformations of the carrier can be input in many different ways, including its calculation in the background with an FEM tool. This instruction document explains step by step, how the whole process can be completed.

## 2 Step by step instructions

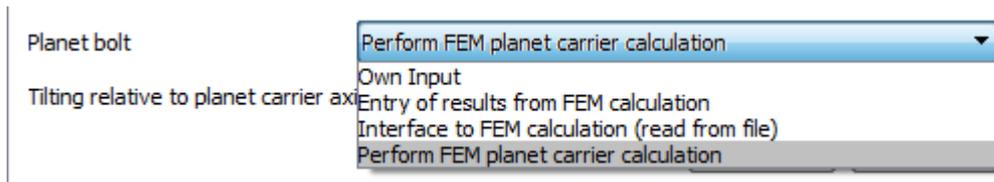
After the user has defined all the necessary inputs for the planetary system, then the process of including the carrier deformation can initiate. The user has to select the Factors tab and then one of the ISO6336-1 Annex E methods:



After that, the user should click the Axis alignment button that appears:



In the next window, the user has the following options in defining the planet's bolt misalignment (dr and dt values):



- Own Input: the user can just type in the values of dr and dt.

- Input results from FEM calculation. Clicking on the Details button, the user can input the coordinates of two nodes on sides I and II of the carrier and their resulting deformations as derived by FEM:

Planet carrier details

FEM model:

Partial load for calculation: 100.0000 %

Reference torque:  $T_{ref}$  25.0669 Nm

Node I, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	mm	↔
Node I, Deformation	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	
Node II, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	mm	↔
Node II, Deformation	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	

OK Cancel

- Read in results of FEM analysis, where clicking the Details button, the user can again input the coordinates of two nodes on sides I and II of the carrier and also give the path to an FEM results file with the deformations of all nodes in the carrier model (ABAQUS and Code\_Aster formats can be used).

Planet carrier details

FEM Solver: Code\_Aster

FEM model:  ...

Partial load for calculation: 100.0000 %

Reference torque:  $T_{ref}$  25.0669 Nm

Node I, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	mm	↔
Node I, Deformation	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	
Node II, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	mm	↔
Node II, Deformation	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	

OK Cancel

- Perform the FEM analysis of the carrier from within KISSsoft. In such a case, the following window opens:

Planet carrier details

Reference torque  $T_{ref}$  25.0669 Nm

Conditions I Conditions II

Configuration

Direction of torsion from side I

Young's modulus E 206000.0000 MPa

Poisson's ratio  $\nu$  0.3000

Default planet carrier  Import planet carrier from Step file

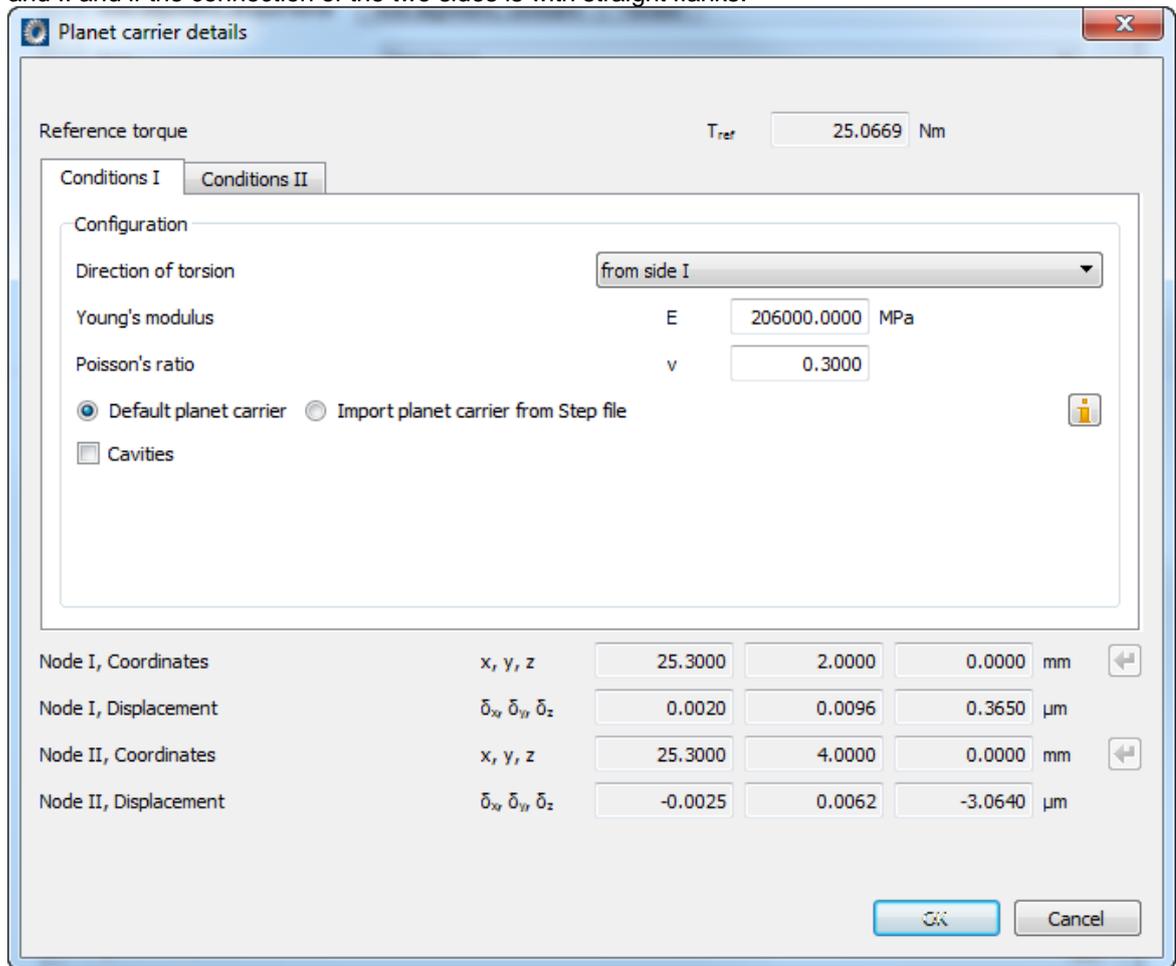
Connection with straight flanks

Cavities

Node I, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	m	↔
Node I, Displacement	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	
Node II, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	m	↔
Node II, Displacement	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	

OK Cancel

Using this window the user can first define the type of carrier to be analysed, i.e. if the default planet carrier will be defined, or if a carrier defined in a step file will be used, if cavities are present on sides I and II and if the connection of the two sides is with straight flanks.



After this selection is finished, then all the necessary parameters for the generation of the 3D model can be entered in the "Conditions II" tab:

Planet carrier details

Reference torque  $T_{ref}$  25.0669 Nm

Conditions I **Conditions II**

Planet carrier		Flange	
Size planet carrier		Size flange	
Planet bolt diameter	$d$ 5.0000 mm	Flange diameter Side I	$d_{f1}$ 0.0000 mm
External diameter coefficient	$f_{vie}$ 1.3500	Flange length Side I	$L_{f1}$ 0.0000 mm
Inner diameter coefficient	$f_{vit}$ 0.6000	Wall thickness Side I	$sw_{f1}$ 0.0000 mm
Rim thickness coefficient	$f_{swt}$ 0.4000		
Rim thickness coefficient	$f_{swt1}$ 0.4000		
Carrier width coefficient	$f_{occ}$ 1.0100		
Connection factor	$f_{dcon}$ 1.0500		
Connection factor	$f_{d1con}$ 1.0000		
Connection length coefficient	$f_r$ 0.1000		
Radius	$r_v$ 0.0000 mm		

Node I, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	m	
Node I, Displacement	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	
Node II, Coordinates	$x, y, z$	0.0000	0.0000	0.0000	m	
Node II, Displacement	$\delta_x, \delta_y, \delta_z$	0.0000	0.0000	0.0000	$\mu\text{m}$	

OK Cancel

The definition of the input parameters can be better understood based on the following sketch (as shown in the KISSsoft help):

Information

N = Number of Planets

$$\begin{aligned} \varnothing W_a &= 2 \cdot a \cdot f_{wa} & r_a &= f_r \cdot a \cdot 2 \cdot \frac{\pi}{N} \\ \varnothing W_i &= 2 \cdot a \cdot f_{wi} & S_{gd} &= f_{gd} \cdot a \cdot 2 \cdot \frac{\pi}{N} \\ S_{wi} &= b \cdot f_{swi} & S_{ge} &= f_{ge} \cdot \frac{(W_a - W_i)}{2} \\ S_{wii} &= b \cdot f_{swii} & S_{gi} &= f_{gi} \cdot \frac{(W_a - W_i)}{2} \\ b_{pc} &= b \cdot f_{bpc} & d_{con} &= d_{apl} \cdot f_{dcon} \\ d_{con} &= 2 \cdot a \cdot f_{dcon} & S_{wgI} &= f_{wgI} \cdot S_{wi} \\ t &= d_{apl} \cdot f_t & S_{wgII} &= f_{wgII} \cdot S_{wii} \end{aligned}$$

I

II

Connector

straight-flanked Connector

Close

The user has also the chance to ask KISSsoft to propose some values for the necessary parameters, using the two sizing buttons:

Planet carrier details

Reference torque  $T_{ref}$  25.0669 Nm

Conditions I Conditions II

Planet carrier

Size planet carrier

Planet bolt diameter  $d$  5.0000 mm

External diameter coefficient  $f_{wa}$  1.3500

Inner diameter coefficient  $f_{wi}$  0.6000

Rim thickness coefficient  $f_{srt}$  0.4000

Rim thickness coefficient  $f_{srt1}$  0.4000

Carrier width coefficient  $f_{dpc}$  1.0100

Connection factor  $f_{con}$  1.0500

Connection factor  $f_{dcon}$  1.0000

Connection length coefficient  $f_r$  0.1000

Radius  $r_v$  0.0000 mm

Flange

Size flange

Flange diameter Side I  $d_{s1}$  0.0000 mm

Flange length Side I  $L_{s1}$  0.0000 mm

Wall thickness Side I  $sw_{r1}$  0.0000 mm

Node I, Coordinates  $x, y, z$  0.0000 0.0000 0.0000 m

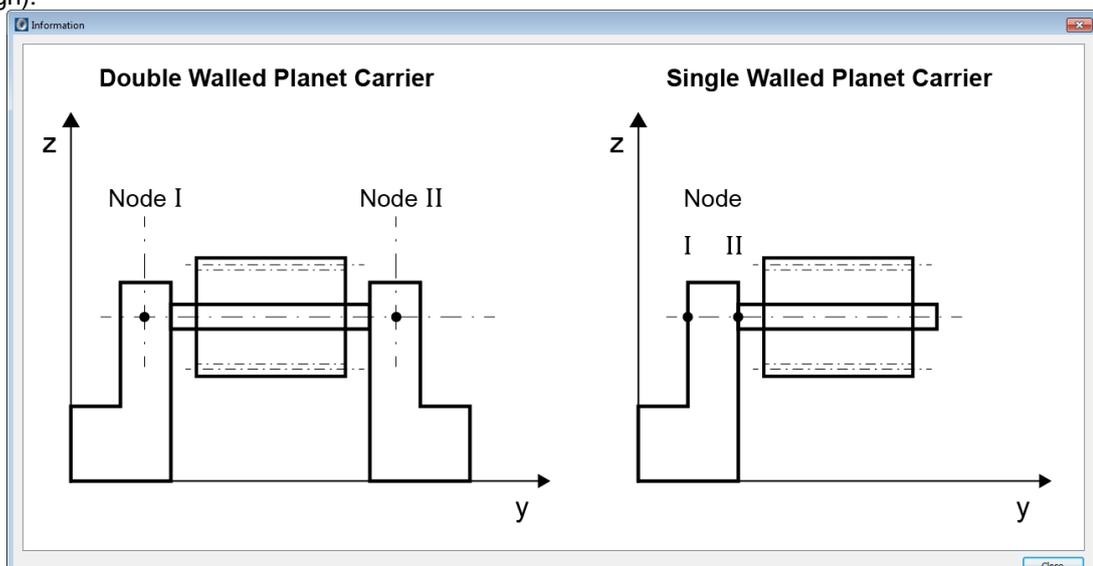
Node I, Displacement  $\delta_x, \delta_y, \delta_z$  0.0000 0.0000 0.0000  $\mu\text{m}$

Node II, Coordinates  $x, y, z$  0.0000 0.0000 0.0000 m

Node II, Displacement  $\delta_x, \delta_y, \delta_z$  0.0000 0.0000 0.0000  $\mu\text{m}$

OK Cancel

Nodes on sides I and II mentioned previously are defined as follows (based on single- or double-walled carrier design):

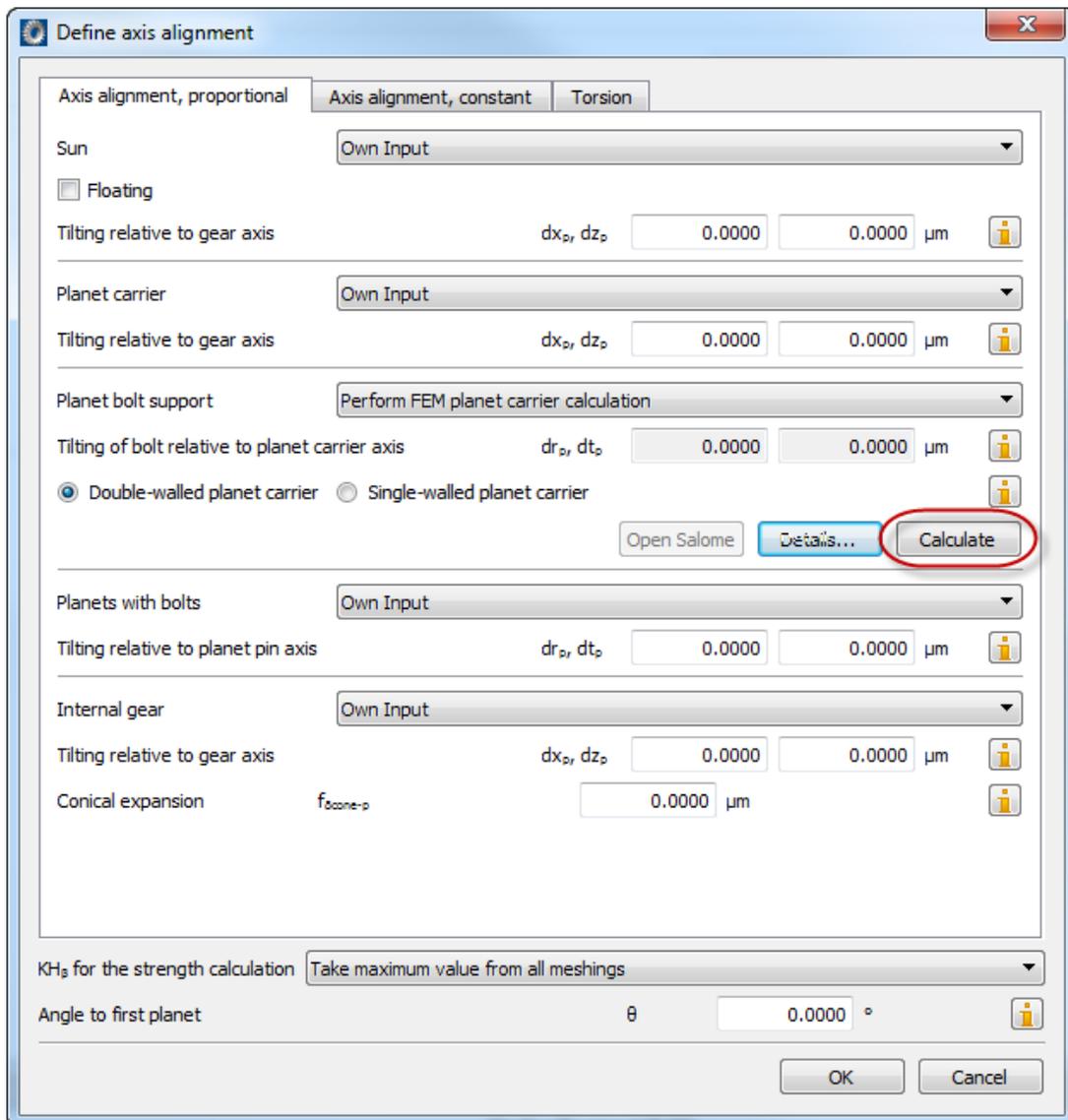


The following points should be noted in the case of the input of a step model of the planet carrier:

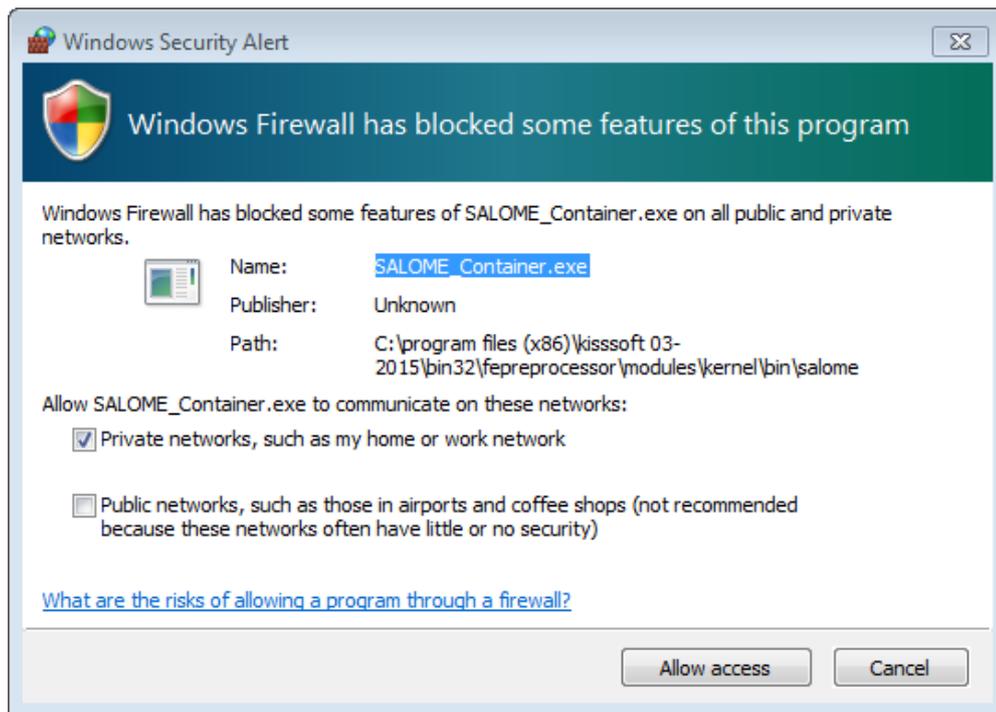
- 1) The geometry should be simplified in such a way as to help the generation of a good mesh, i.e. any details that do not have an effect on the deformation of the carrier should be removed.

- 2) The planet carrier should not include any planet bolts, since they will be generated automatically.
- 3) The planet bolt and the flange inner diameters should be given with adequate accuracy, so as to generate the complete model correctly.
- 4) The planet carrier is hold in place (clamped) at the cylindrical area defined by the flange diameter and the start and end clamping positions.
- 5) The planet bolts are cylinders with the given diameter and length defined by the coordinates of their start and end positions.
- 6) It is strictly advised to check the generated mesh inside Salome after the solution, in order to make sure that it correctly represents the input geometry and boundary conditions.

If any of the last three options are selected, the user has to click the Calculate button to take the input into consideration:

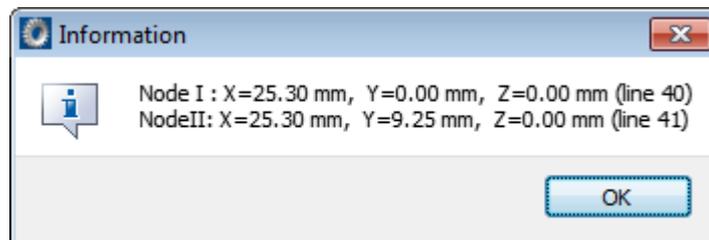


In case the last option was selected (perform the FEM analysis of the carrier from within KISSsoft), the program will give first any warnings or errors regarding the input parameters. If no errors are present, then KISSsoft will call in the background the FEM tool that installs with KISSsoft and perform the calculation. It should be noted here that the first time this FEM tool is used, some messages will appear requesting access through the firewall, as for example:

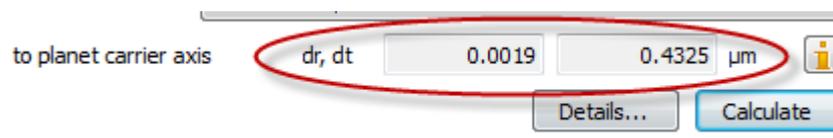


It is not necessary to allow access through the firewall for the FEM tool to work correctly, hence the user can press Cancel.

After the calculation is completed correctly, the resulting coordinates of the nodes selected by the FEM tool are given for validation:



And finally the resulting dr and dt are presented:



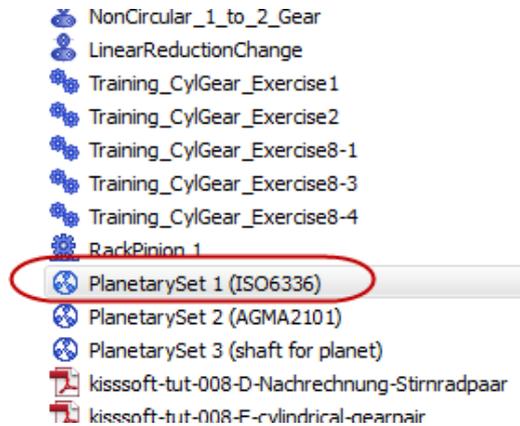
This result can be subsequently used in the planetary system analysis.

### 3 General comments

- Further details on the FEM tool used by KISSsoft are given in the KISSsoft manual.
- A separate instructions document is available describing the necessary steps to access the 3D model, the FEM mesh and the FEM results of the planet carrier, as derived in the background by the FEM tool.
- The info buttons  in all the above windows can give information on various definitions on the process, as for example the definition of dr and dt misalignments, or the definition of the parameters for the 3D model of the planet carrier.

## Annex 1. Comparison between the deformations of a single-sided and double-sided planet carrier

In order to present the significance of taking into account the carrier deformation in planetary stage design, we present here the resulting carrier deformation for a single-sided and a double-sided carrier. The calculation is based on example “PlanetarySet 1 (ISO6336)” of the standard KISSsoft examples:



Following we can see the inputs and the results for the two different planet carrier types:

**Double-sided carrier:**

Planet carrier details

Reference torque  $T_{ref}$  25.0669 Nm

Conditions I Conditions II

Planet carrier

Size planet carrier

Planet bolt diameter  $d$  3.5042 mm

External diameter coefficient  $f_{vis}$  1.3500

Inner diameter coefficient  $f_{wi}$  0.6000

Rim thickness coefficient  $f_{srit}$  0.4000

Rim thickness coefficient  $f_{srit1}$  0.4000

Carrier width coefficient  $f_{cpc}$  1.0500

Connection factor  $f_{con}$  1.0500

Connection factor  $f_{cicon}$  1.0000

Connection length coefficient  $f_r$  0.1000

Radius  $r_v$  0.0000 mm

Flange

Size flange

Flange diameter Side I  $d_{r1}$  30.3600 mm

Flange length Side I  $L_{r1}$  2.0000 mm

Wall thickness Side I  $sw_{r1}$  2.0000 mm

Node I, Coordinates  $x, y, z$  25.3000 2.0000 0.0000 mm

Node I, Displacement  $\delta_x, \delta_y, \delta_z$  -0.0027 0.0072 -0.9341  $\mu\text{m}$

Node II, Coordinates  $x, y, z$  25.3000 11.2500 0.0000 mm

Node II, Displacement  $\delta_x, \delta_y, \delta_z$  -0.0026 0.0051 -1.4071  $\mu\text{m}$

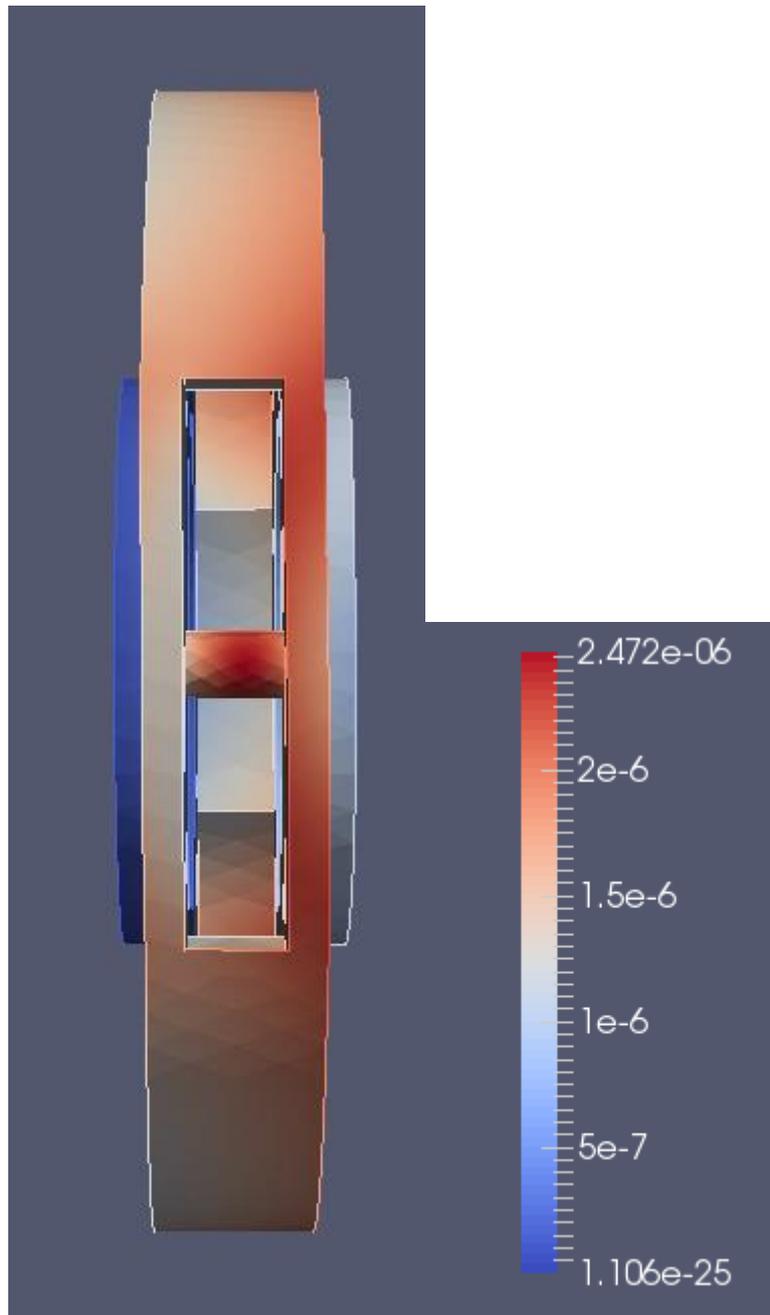
OK Cancel

Result:

Tilting of bolt relative to planet carrier axis  $dr_o, dt_o$  0.0001 0.4729  $\mu\text{m}$

Double-walled planet carrier  Single-walled planet carrier

Deformed shape:



**Single-sided carrier:**

Planet carrier details

Reference torque  $T_{ref}$  25.0669 Nm

Conditions I Conditions II

Configuration

Direction of torsion from side I

Young's modulus E 206000.0000 MPa

Poisson's ratio  $\nu$  0.3000

Default planet carrier  Import planet carrier from Step file

Cavities

Node I, Coordinates	$x, y, z$	25.3000	2.0000	0.0000	mm
Node I, Displacement	$\delta_x, \delta_y, \delta_z$	0.0020	0.0096	0.3650	$\mu\text{m}$
Node II, Coordinates	$x, y, z$	25.3000	4.0000	0.0000	mm
Node II, Displacement	$\delta_x, \delta_y, \delta_z$	-0.0025	0.0062	-3.0640	$\mu\text{m}$

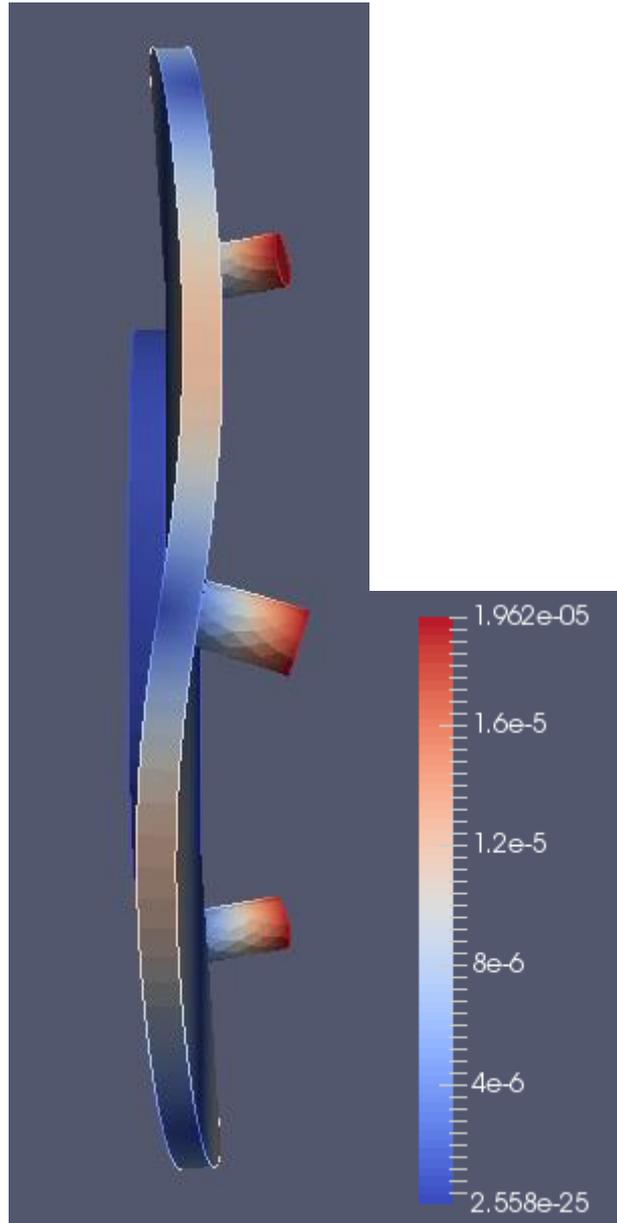
OK Cancel

Result:

Tilting of bolt relative to planet carrier axis  $dr_p, dt_p$  -0.0165 12.4303  $\mu\text{m}$

Double-walled planet carrier  Single-walled planet carrier

Deformed shape (Note: The same scaling factor to visualize the deformation is used as in the picture of the double sided carrier):



From the above results it is clear that the deformation of the single-sided planet carrier is bigger than the double-sided, mainly due to the “wave” like deformation of the carrier side (the deformed shapes on the above pictures are plotted using the same scaling factor). Hence it is obvious that the deformation of the carrier has a significant influence on the planetary stage design, with this influence being stronger for the single-sided planet carrier.